

Transmission Lines in Metamaterial

A Route to Design Artificial Metamaterials

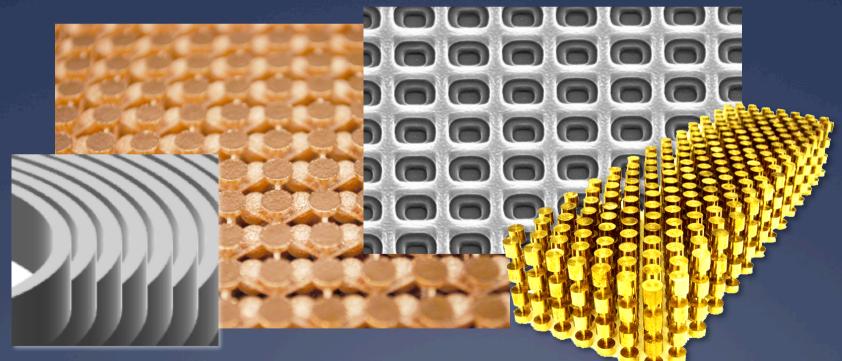
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Outline

- Introduction Artificial materials
- ☐ Transmission line approach for metamaterial design
- Design examples
- Conclusions

What Are Metamaterials?

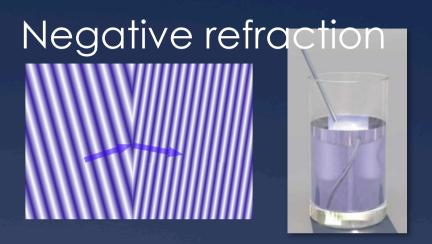
- Artificial materials composed of subwavelength elements
- Exhibit unusual electromagnetic properties which do not exist in nature



Macroscopically homogeneous media

Unusual Properties





Backward* Leaky-Wave Zeroth-order resonance

n = 0

 $n = \pm 1$

 $n = \pm 2$

Reverse Doppler effect

 $n = \pm 3$

4

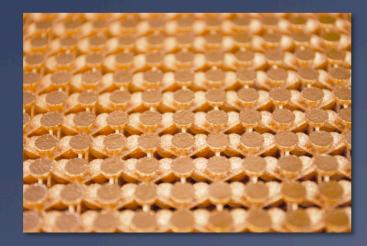
Designing Macroscopic Properties

- Material
 Material properties
- Shape Inductive/capacitive resonance
- ArrangementCouplings, periodicity

affect macroscopic material properties very much

Characterization

- ✓ Materials
- ✓ Topology
- ✓ Dimension
- ✓ Wavelength



- ✓ Negative/positive permittivity and permeability
- ✓ Dispersion
- ✓ Band structure
- ✓ Anisotropy
- ✓ Chirality

$$D = \overline{\varepsilon}E + \overline{\xi}H$$

$$\boldsymbol{B} = \overline{\mu}\boldsymbol{H} + \zeta \boldsymbol{E}$$

Can We Go Backward?

- ✓ Materials
- ✓ Topology
- ✓ Dimension
- ✓ Wavelength



- ✓ Negative/positive permittivity and permeability
- ✓ Dispersion
- ✓ Band structure
- ✓ Anisotropy
- ✓ Chirality

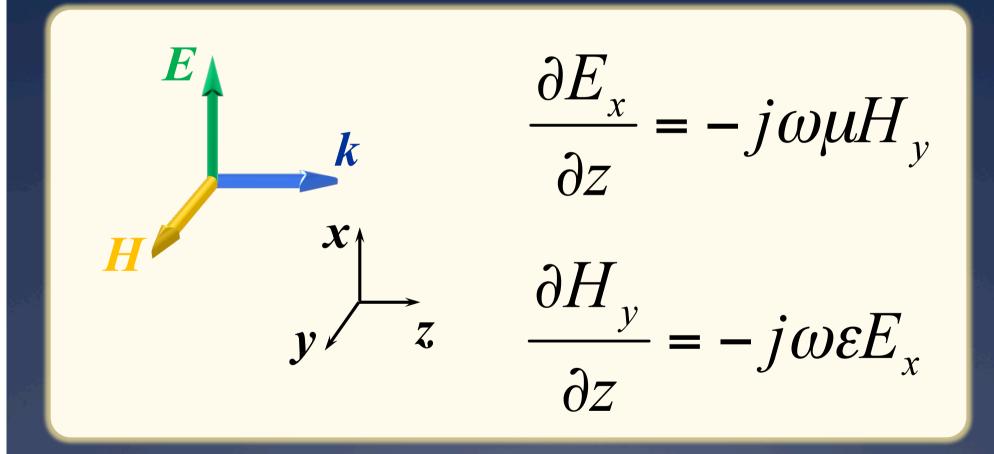


$$D = \overline{\varepsilon}E + \overline{\xi}H$$

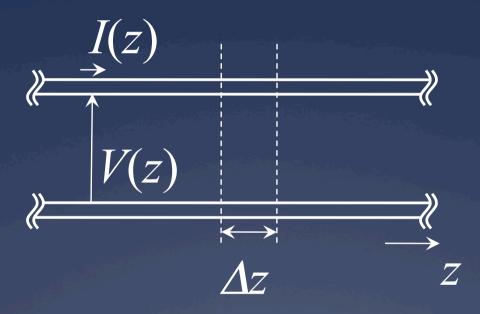
$$\boldsymbol{B} = \overline{\mu}\boldsymbol{H} + \overline{\zeta}\boldsymbol{E}$$

Transmission Line Concept A Route to Design Artificial Materials

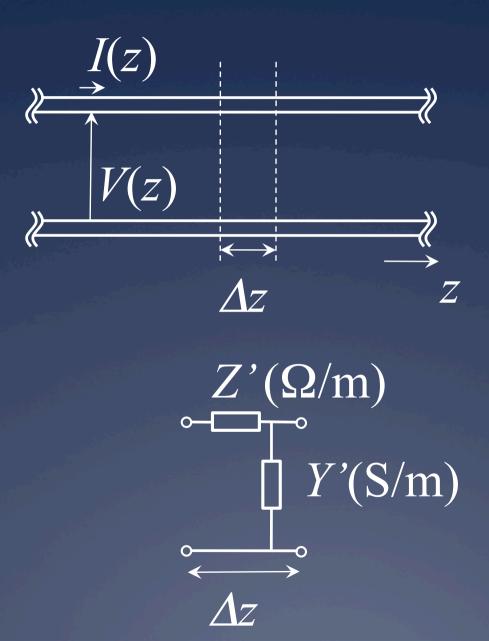
Plane Wave



Transmission Line



Transmission Line



Kirchhoff's Laws

$$\begin{array}{c}
I_{n} \downarrow Z' \\
V_{n} \downarrow Y' \downarrow \downarrow V_{n+1}
\end{array}$$

$$\Delta z$$

$$\frac{V_{n+1} - V_n}{\Delta z} = -Z'I_n$$

$$\frac{I_{n+1} - I_n}{\Delta z} = -Y'V_{n+1}$$

Telegrapher's Equations

$$\begin{array}{c|c}
I_{n} & Z' & I_{n+1} \\
V_{n} & Y' & V_{n+1} \\
\hline
\Delta z
\end{array}$$

$$\Delta z \to 0$$

$$\frac{\partial V}{\partial z} = -Z'I$$

$$\frac{\partial I}{\partial z} = -Y'V$$

(E,H) vs. (V,I) Correspondence

Maxwell's Eqs.

$$\frac{\partial E_x}{\partial z} = -j\omega \mu H_y$$

$$\frac{\partial H_{y}}{\partial z} = -j\omega \varepsilon \widehat{E}_{x};$$

Telegrapher's Eqs.

$$\frac{\partial V}{\partial z} = -Z'I$$

$$\frac{\partial I}{\partial z} = -Y'V$$

(ϵ,μ) vs. (Z',Y') Correspondence

Maxwell's Eqs.

$$\frac{\partial E_x}{\partial z} = -ij\omega \mu H_y$$

$$\frac{\partial H_{y}}{\partial z} = -i \int \omega \varepsilon E_{x}$$

Telegrapher's Eqs.

$$\frac{\partial V}{\partial z} = -Z'I$$

$$\frac{\partial I}{\partial z} = \underbrace{(Y')}V$$

Example: Right-Handed Material

$$\varepsilon = \frac{Y'}{j\omega} \qquad \mu = \frac{Z'}{j\omega}$$

$$Z' = j\omega L'$$

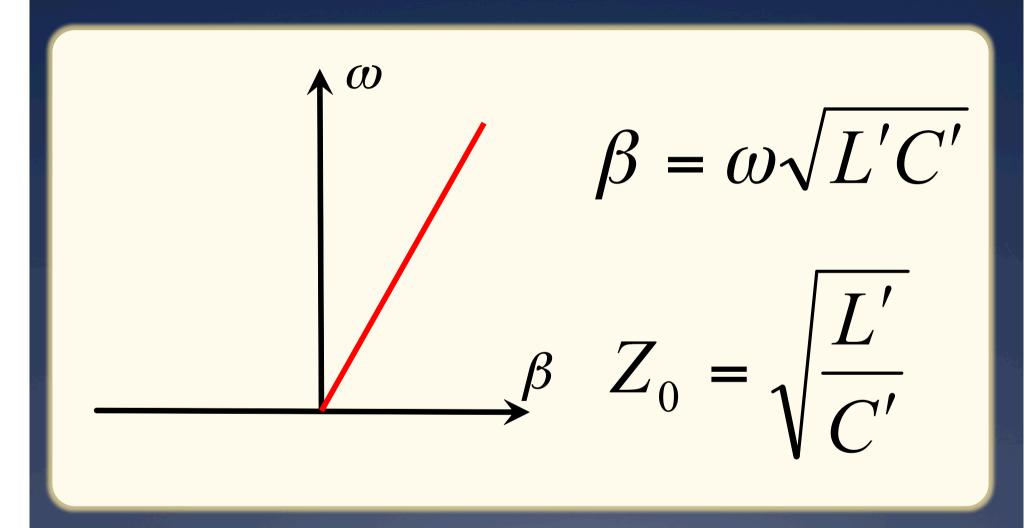
$$Y' = j\omega C'$$

$$\Delta z$$

$$\varepsilon = C' \text{ (F/m)}$$

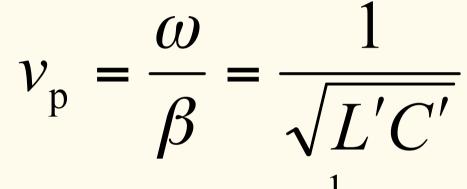
$$\mu = L' (H/m)$$

Dispersion Relation and Impedance



Phase and Group Velocities

$$\beta = \omega \sqrt{L'C'}$$



$$v_{\rm g} = \left(\frac{\partial \beta}{\partial \omega}\right)^{-1} = \frac{1}{\sqrt{L'C'}}$$

Plane Wave

$$\frac{d^{2}E_{x}}{dz^{2}} + k^{2}E_{x} = 0$$

$$\frac{d^{2}H_{y}}{dz^{2}} + k^{2}H_{y} = 0$$

$$j\omega\varepsilon, j\omega\mu$$

$$k = \omega\sqrt{\varepsilon\mu}$$

$$E_{x} = E_{x}^{+}e^{-jkz} + E_{x}^{-}e^{jkz}$$

$$H_{y} = H_{y}^{+}e^{-jkz} + H_{y}^{-}e^{jkz}$$

$$\eta = E_{x}^{+}/H_{y}^{+} = -E_{x}^{-}/H_{y}^{-} = \sqrt{\mu/\varepsilon}$$

$$S_{z} = E_{x}H_{y}^{*}$$

Transmission Line

$$\frac{d^2V}{dz^2} - \gamma^2 V = 0$$

$$\frac{d^2I}{dz^2} - \gamma^2 I = 0$$

$$Y', Z'$$

$$\gamma = \sqrt{Z'Y'}$$

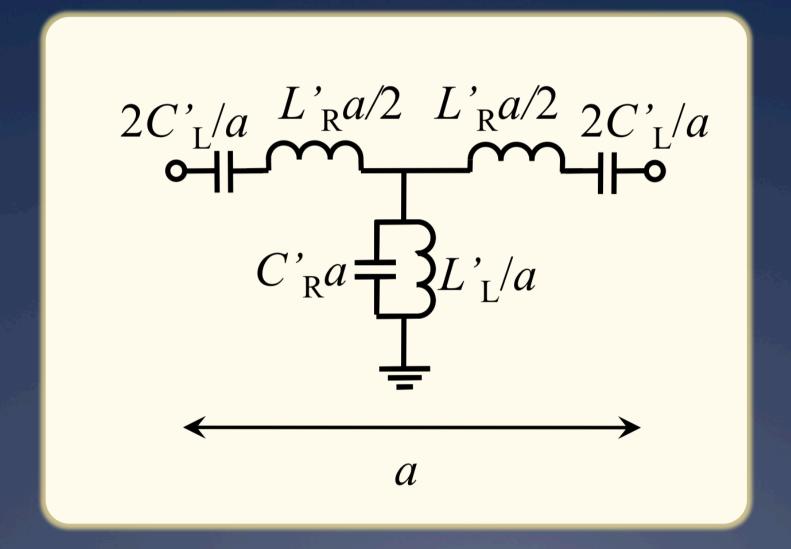
$$V = V^+ e^{-\gamma z} + V^- e^{\gamma z}$$

$$I = I^+ e^{-\gamma z} - I^- e^{\gamma z}$$

$$Z_0 = V^+ / I^+ = -V^- / I^- = \sqrt{Z'/Y'}$$

$$P = VI^*$$

Example 2: Left-Handed Materials



Periodic structure

Dispersion Relation

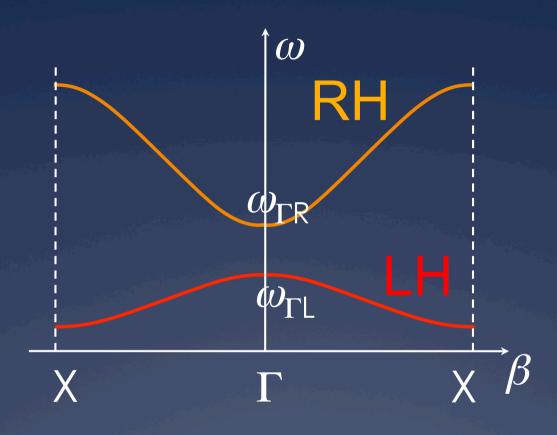
$$ZC'_{L}/a \xrightarrow{L'_{R}a/2} \xrightarrow{L'_{R}a/2} 2C'_{L}/a$$

$$C'_{R}a \xrightarrow{L'_{L}/a} \xrightarrow{L'_{L}/a}$$

$$\cos \beta a = 1 + Z(\omega)Y(\omega)$$

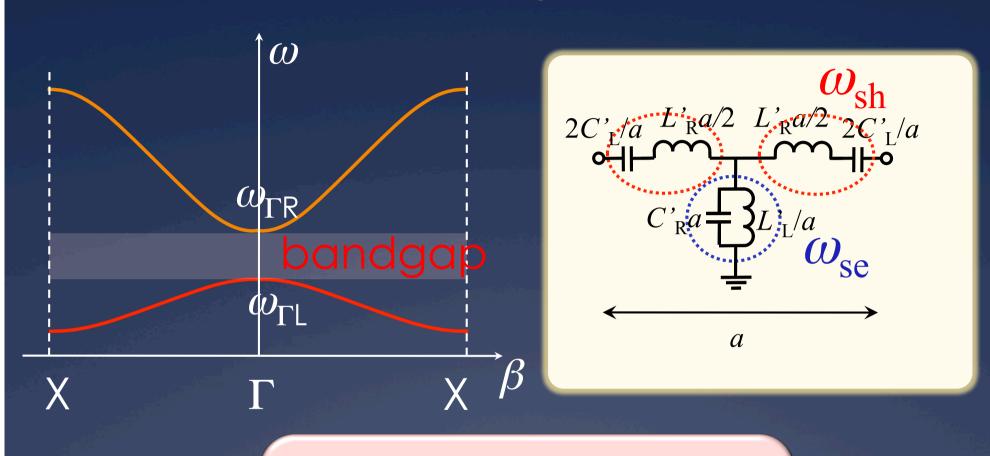
$$Z(\omega) = \frac{1}{2} \left(\frac{1}{j\omega C_{L}} + j\omega L_{R}\right) \quad Y(\omega) = \frac{1}{j\omega L_{L}} + j\omega C_{R}$$

Dispersion Characteristics (Theory)



$$\cos \beta a = 1 + Z(\omega)Y(\omega)$$

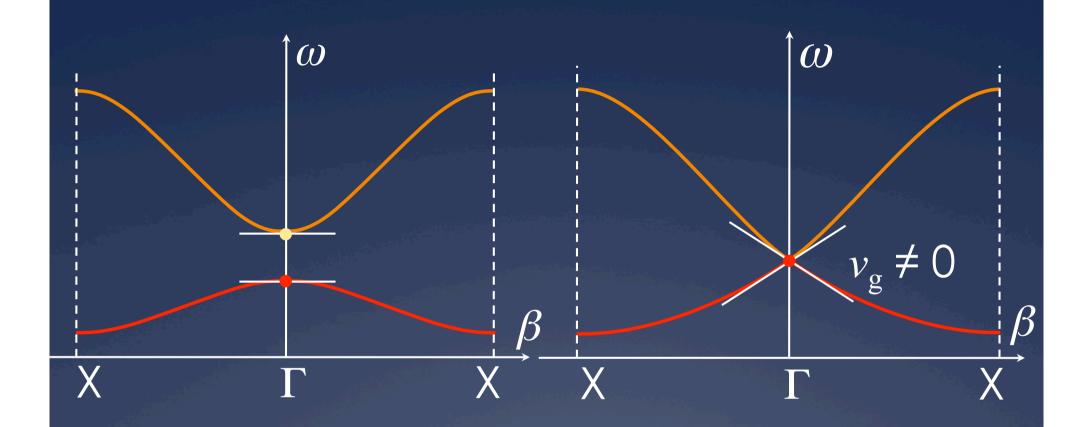
Γ-Point Frequencies



$$\omega_{\Gamma R} = \max(\omega_{se}, \omega_{sh})$$

$$\omega_{\Gamma L} = \min(\omega_{se}, \omega_{sh})$$

Closing the Bandgap

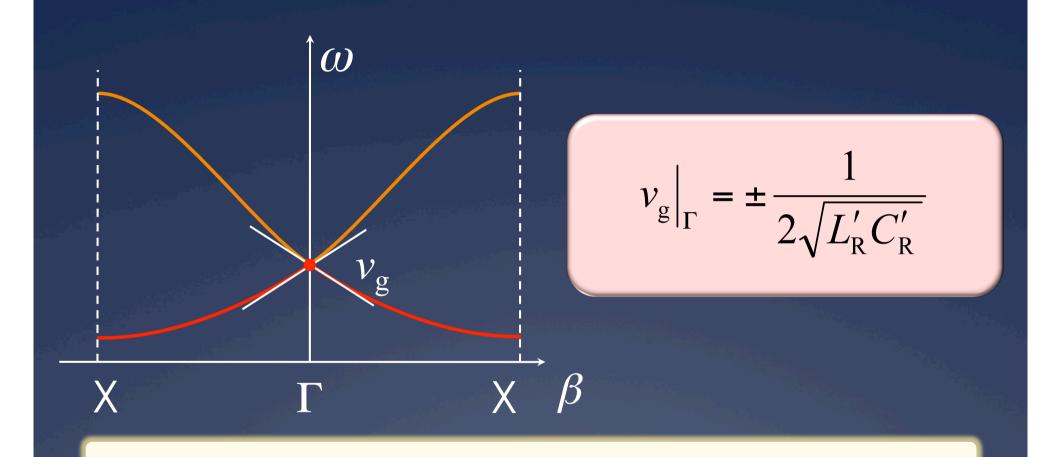


$$\omega_{\rm se} \neq \omega_{\rm sh}$$

$$\omega_{\rm se} = \omega_{\rm sh}$$

balanced condition

Non-Zero Group Velocity at Γ-Point



For
$$L'_{\rm R} = \mu_0$$
, $C'_{\rm R} = \varepsilon_0$,

$$v_{\rm g} = \pm \frac{c_0}{2}$$

Bloch Impedance

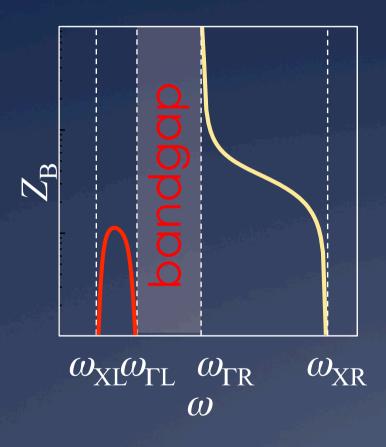
$$2C'_{L}/a \qquad L'_{R}a/2 \qquad L'_{R}a/2 \qquad 2C'_{L}/a$$

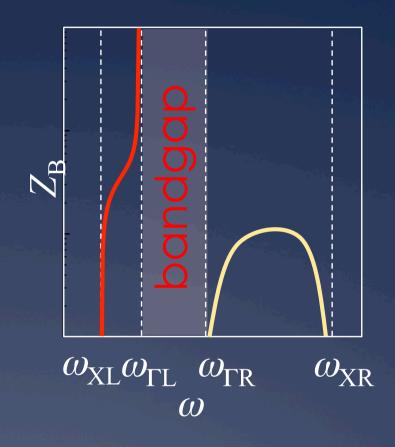
$$C'_{R}a = \frac{1}{2}L'_{L}/a$$

$$a$$

$$Z_{\rm B} = Z_{\rm L} \sqrt{\frac{\frac{\omega^2}{\omega_{\rm se}^2} - 1}{\frac{\omega^2}{\omega_{\rm sh}^2} - 1}} - \frac{\omega_{\rm L}^2}{4\omega^2} \left(\frac{\omega^2}{\omega_{\rm se}^2} - 1\right)^2 \qquad Z_{\rm L} = \sqrt{\frac{L_{\rm L}}{C_{\rm L}}}$$

Frequency Dependence of Z_B

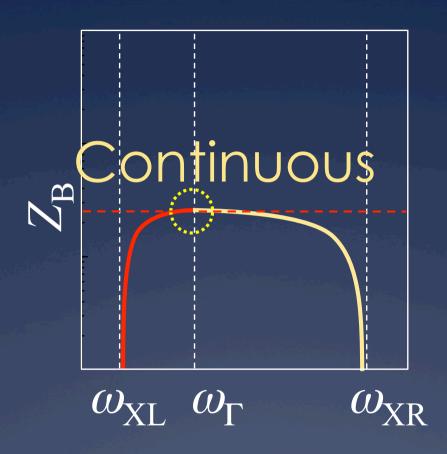




$$\omega_{\rm se} < \omega_{\rm sh}$$

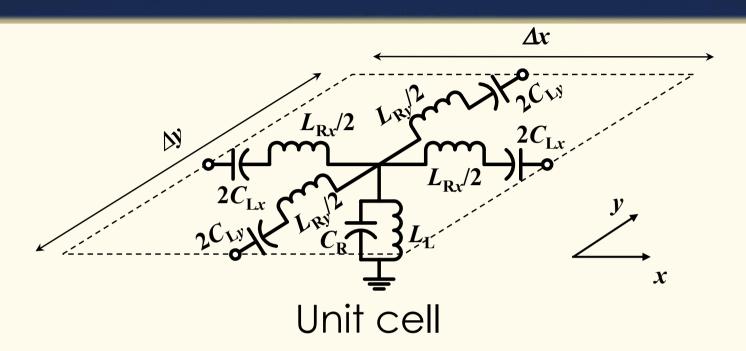
$$\omega_{\rm se} > \omega_{\rm sh}$$

Continuity of Z_B at the Γ -Point



$$\omega_{\rm se} = \omega_{\rm sh}$$

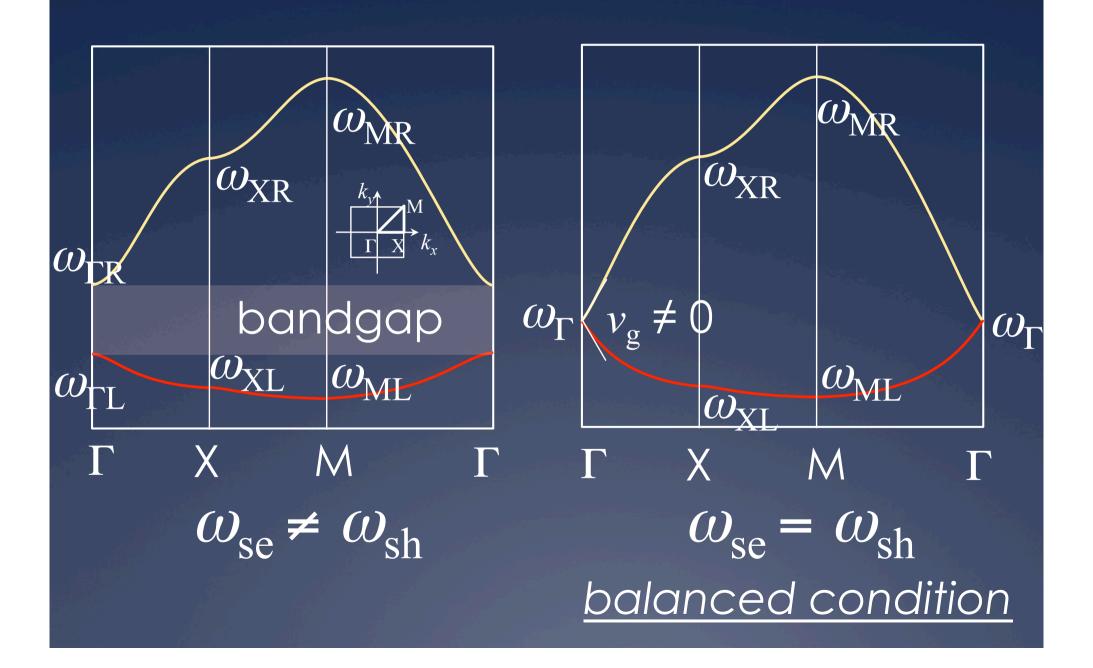
2D Extension



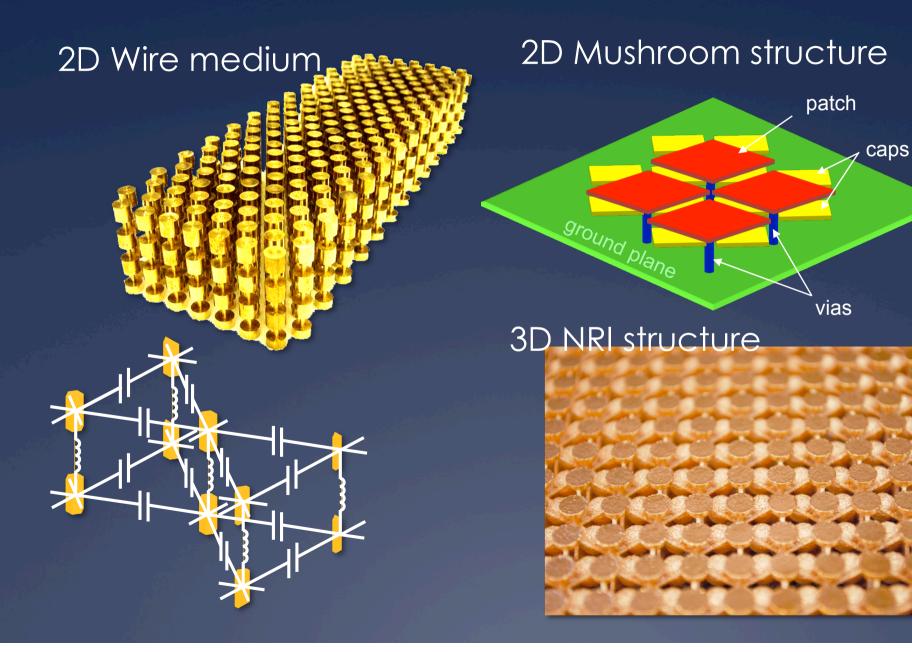
Dispersion Relation

$$\frac{\left(e^{-jk_x a} - 1\right)^2}{e^{-jk_x a}} + \frac{\left(e^{-jk_y a} - 1\right)^2}{e^{-jk_y a}} - 2Z(\omega)Y(\omega) = 0$$

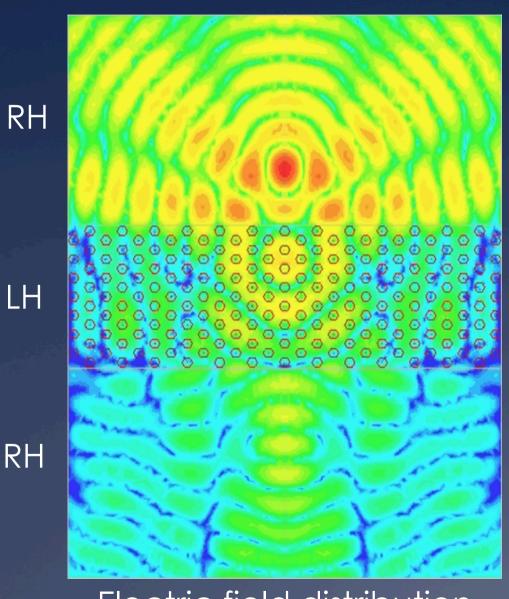
Dispersion Characteristics (2D)



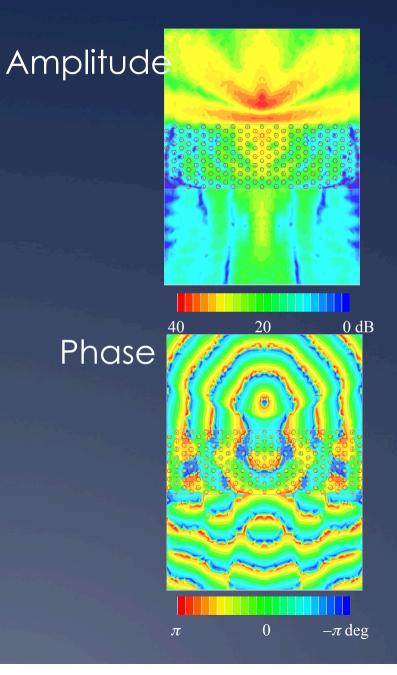
Implementation Examples



NRI Lens (Full-Wave Simulation)



Electric field distribution



Conclusions

- The transmission line (TL) approach has been introduced as a route to design and engineer metamaterials
- The TL model can be an abstract form of artificial material revealing physical insight of wave propagation
- The TL model well describes properties of left -handed metamaterials including the band structure and impedance
- The concept can be extendable to 2D/3D structures
- The concept is scalable from microwave to optical frequency range

